



## A Digital Constant Current Power LED Driver

Author: Stephen Bowling  
Microchip Technology Inc.

### INTRODUCTION

This document describes a power LED driver solution using the PIC12HV615 microcontroller (MCU). The PIC12HV615 is an 8-pin MCU with many integrated analog features. The LED driver circuit is a buck (step-down) solution and the circuit presented here can operate from most any input voltage source as long as it exceeds the forward voltage of the LEDs to be driven.

A proportional-integral (PI) controller algorithm is used to regulate the LED current to a constant value. The PI controller is executed at a rate of 976 Hz, leaving plenty of CPU time available for other tasks. Although this sample rate would provide inadequate control response for most power supply applications, it works well for LED applications because the LED presents a constant load to the power stage. Therefore, the controller does not need to make frequent adjustments.

The LED current is sampled using a resistor in series with the source of the MOSFET in the buck circuit and amplified using a single op amp. The LED current is sampled using one of the available ADC inputs on the PIC12HV615. The Enhanced Capture Compare PWM (ECCP) module of the MCU is used in PWM mode to drive the buck circuit. Since the MCU has an internal voltage regulator and 8 MHz oscillator, very few external components are required to complete the circuit.

### CIRCUIT DESCRIPTION

A detailed schematic of the circuit is provided in Figure B-1. A buck topology is used with the LED load referenced to the input voltage rail. The buck topology allows the LED to be in series with the inductor at all times and limit the current ripple. Therefore, an output capacitor is not required as it would be for a voltage regulator circuit. However, an output capacitor is shown in the schematic and can optionally be used to lower the required value of the inductor.

In order to select an inductor value for the buck circuit, we need to know some basic operating parameters. For calculation purposes, we will assume that the circuit will drive a single 1W power LED. The typical

drive current for this type of LED would be 350 mA and a typical forward voltage would be 3.5V. Secondly, we will assume that the circuit input voltage is 12V.

The inductor value will be chosen to allow a maximum current ripple of +/- 20%. The eye will not be able to perceive this current ripple since the switching frequency is much faster than can be detected. Considering this fact, you might be tempted to further increase the allowable current ripple to reduce the inductor value. However, the +/- 20% limit is a rule of thumb to minimize efficiency losses in the LED. You will want to check the LED manufacturer's data sheet to verify the maximum peak current.

The switching frequency of the buck regulator is chosen to be 125 kHz. This frequency was chosen based on the selected operating frequency of the MCU and the resulting control resolution that can be obtained from the hardware PWM module. When operated from the internal 8 MHz RC oscillator, the ECCP module can provide 6 bits (64 steps) of duty cycle resolution at 125 kHz. If this control resolution is not sufficient, the PWM frequency can be lowered or the MCU can be operated with an external oscillator circuit to provide a higher operating frequency.

A summary of the operating parameters used for design calculations is provided in Table 1 below.

**TABLE 1: BUCK REGULATOR OPERATING PARAMETERS**

Parameter	Value
Input Voltage, $V_{IN}$	12V
LED Forward Voltage, $V_f$	3.5V
LED Current, $I_f$	0.35A
Current Ripple, $\Delta I$	+/- 20%
Switching Frequency, $f_{sw}$	125 kHz

**EQUATION 1: INDUCTOR VALUE**

$$L = \frac{(V_{in} - V_f)}{\Delta I} \bullet t_{on} = \frac{V_f}{\Delta I} \bullet t_{off}$$

**EQUATION 2: INDUCTOR CHARGE TIME**

$$t_{on} = \frac{1}{f_{sw}} \bullet \frac{V_f}{V_{in}}$$

The inductor value, L, can be calculated using Equation 1 and Equation 2. The inductor value should be at least 128  $\mu$ H to achieve the desired current maximum current ripple. A standard inductor value of 150  $\mu$ H was chosen for the design based on this calculation.

A 0.56 ohm sensing resistor is used to measure the LED current. The sense resistor is placed in series with the source of the power MOSFET. The resistor value was chosen to provide low-power dissipation, but this value also provides a very low output voltage at typical operating currents.

A single op amp is used in a non-inverting amplifier configuration to increase the current feedback signal amplitude. A larger resistor could be used to eliminate the gain stage, but this would result in significant power dissipation. More important, the resistor power dissipation would reduce the overall efficiency of the LED driver.

The feedback components of the op amp are selected to provide a gain of 11. This gain value will provide a nominal feedback voltage of 2V at 350 mA drive current and 4V at 700 mA drive current.

Because of the location of the sense resistor in the circuit, the current feedback signal is present only when the MOSFET is turned on and charging the inductor. Since the feedback signal is discontinuous, a simple peak hold circuit using a Shottky diode is used at the output of the current sense amplifier. The component values of the peak hold circuit are chosen to provide a low pass filter with a very low cutoff frequency, which averages the current feedback signal. To ensure that the current can be properly regulated using the software PI controller, the cutoff frequency is chosen to be 1/10th the value of the current sample rate.

The Enhanced Capture Compare PWM (ECCP) module on the PIC12HV615 is used to control the buck regulator MOSFET. The output of the current sense amplifier and peak hold circuit is connected to input AN0 of the PIC12HV615 ADC.

A dropping resistor is used between the input voltage rail of the circuit delivered by J1 and the VDD pin of the PIC12HV615. This resistor must be sized to provide the operating current for the internal shunt regulator, plus the expected operating current of the device. Refer to the PIC12HV615 (DS41302) data sheet to determine the value of this resistor.

Connector J2 allows the PIC12HV615 device to be programmed using a MPLAB® ICD 2 or PICkit™ 2 device programmer. Jumpers J3 and J4 must be removed during device programming. (See schematic diagram, Figure B-1.)

## SOFTWARE DESCRIPTION

The CCS PICC™ C compiler was used to develop the source code for this application. The PICC C compiler has a variety of built-in library functions that allow the user to rapidly configure the I/O pins and peripherals of the MCU.

The Setup() function configures Timer2, the ECCP module, and the ADC. The Timer2 module is used along with the ECCP module to produce a PWM signal. Timer2 also provides software interrupts that schedule ADC conversions and calculation of the PI control algorithm.

The Timer2 output postscaler is used to reduce the frequency of interrupts to the CPU. With the 1:16 postscaler option the interrupt frequency is 7812 Hz. A count variable, Count1msec, is incremented each time a Timer2 interrupt occurs. An ADC conversion is performed and the PI algorithm is executed after every eight Timer2 interrupts. The PI calculation period is 1.025 msec, or 976 Hz. The ADC conversion and PI calculation is scheduled by setting a flag bit, Event1msec, in the ISR. The flag is responded to in the main software loop to avoid consuming time in the ISR.

A `typedef` is used to create a data type for the PI data structure. A pointer to the data structure is passed to the actual PI function. This implementation allows multiple control loops to be created and called in the application, if desired. The data structure contains all the variables associated with a particular control loop.

The PICC C compiler defines the long data type as a 16-bit integer and the int data type as an 8-bit integer. Most values in the PI data structure are declared as long values to provide adequate calculation resolution. The gain values and output limit can be declared as 8-bit values to conserve RAM space.

### EXAMPLE 1: CODE EXAMPLE

```
typedef struct {
    unsigned char      Kp;
    unsigned char      Ki;
    unsigned char      OutMax;
    signed long        Setpoint;
    signed long        Feedback;
    signed long        Error;
    signed long        Integral;
    signed long        Output;
    int1              Saturated;
} tPIParams;
```

The equations required to execute a PI controller are shown in Equation 3. In this control system, the ADC conversion provides the amount of measured LED current. The PI controller calculates an error based on this measured feedback value and the chosen operating current. The PI controller output is then used to set the duty cycle for the buck converter. The operation and behavior of the PI controller is described in further detail below.

### EQUATION 3: PI CONTROLLER

$$\text{Error} = \text{Setpoint} - \text{Feedback}$$

$$\text{Integral} = \text{Integral} + \text{Error}$$

<b>PROPORTIONAL TERM</b>	<b>INTEGRAL TERM</b>
	
$\text{Output} = \frac{K_p \cdot \text{Error} + K_i \cdot \text{Integral}}{K}$	

First an error term is calculated. This is simply the difference between the desired system output value (Setpoint) and the actual output value (Feedback). In this current regulator application, the ADC will provide a sample value corresponding to the actual output current and a setpoint value will be initialized that represents the desired output current.

If the error term is small enough, then no further calculations are performed. This error windowing function saves a significant amount of CPU bandwidth. Often, little or no change of the PWM duty cycle is required once the power LED reaches a steady state operating point.

The proportional term of the controller multiplies the calculated error by a gain value. The proportional term provides a system response that is proportional to the amount of error. If the output current is very near the desired value, the proportional term of the controller will provide very little response to correct the error. If the output current is much greater or much less than the desired output value, then the proportional term of the controller will produce a very big response to correct the large error.

The goal is to reduce the error to zero and the PI control algorithm cannot do this with just a proportional term. With only proportional control, the output of the PI controller equation will be zero when the error is zero!

The integral part of the controller comes to the rescue and provides an output response that keeps the system at the desired setpoint under steady state conditions.

The integral part of the PI controller works by adding the calculated error to a running sum each time the PI controller is executed. This sum, or integrated error, is multiplied by a gain coefficient to produce the integral response of the controller. Dynamically, this causes a small system error to accumulate over time and produce a larger response. Therefore, the integral part of the controller will correct small steady state errors.

As the error converges to zero, the integral term will converge to a value that produces the correct control response to keep the system at the desired setpoint. As stated earlier, the proportional output of the controller will produce little or no response when the error is close to zero. So, it is the integral term that maintains the DC response that keeps the system operating at the desired setpoint.

The error is not added to the integral term under two conditions. First, the error will not be added if the PI controller output has reached its maximum or minimum allowable value. In this application, the minimum output duty cycle is 0 and the maximum is a duty cycle near 100%. If a maximum or minimum duty cycle limit has been reached, the output of the PI controller is restricted to that value and a flag is set to indicate that the controller is in a saturation condition. The saturation check avoids a condition known as "integral windup". If the integral term is allowed to accumulate when the controller is saturated, then very erratic results will occur when the controller comes out of saturation.

Secondly, the error value is not added to the integral term when the integral value has reached a limit of +/- 32000. This limit check keeps the integral variable within the limits of a 16-bit signed integer and avoids the use of extra RAM locations.

As shown in the formulas provided in Equation 3, the output calculation for the controller divides the proportional and integral terms by a constant K. K is an integer value that sets the overall gain of the controller and also sets the resolution of the  $K_p$  and  $K_i$  gain values. This constant allows fractional gains to be utilized.

The PI controller can be tuned experimentally by finding the maximum  $K_p$  value that can be used without oscillations. The output of the ECCP module or the output of the current sensing circuit is observed as  $K_p$  is adjusted to confirm that no oscillations are present. The  $K_i$  gain value is set to 0 at this time, so the current output will not increase to the desired setpoint.

Once a suitable for  $K_p$  has been found,  $K_i$  can be slowly increased to find a value that will make the system error decrease to 0. Usually, the  $K_i$  value is set to a value much less than the value of  $K_p$ . When  $K_i$  is too small, the system will take longer to reach the desired setpoint. When  $K_i$  is too big, the system will over-correct and oscillations will occur.

## GOING FURTHER..

This application note presents only the digital current control software required for the LED. At a minimum, the PIC12HV615 must monitor the LED current. In addition, other signals can be monitored depending on the application requirements. The schematic shown in Figure B-1 has extra MCU inputs available that could be used to monitor the input bus voltage, a temperature sensor, or a push-button. In particular, it might be desirable to monitor the temperature of the power LED with a temperature sensor. The digital control loop can then automatically reduce the current drive level to protect the lifetime of the power LED.

In particular, it might be desirable to monitor the temperature of the power LED with a temperature sensor. LEDs have very long lifetimes, but only if the temperature is kept within limits. It is not always possible to ensure that the mechanical installation of the LED will provide enough heat sinking to keep the LED temperature within specifications.

With electronic thermal management, the LED drive current can be reduced if the maximum LED temperature is exceeded. Therefore, the LED lighting system will always produce the maximum amount of light allowed by the mechanical installation and the lifetime of the LED will be maximized.

## HARDWARE RESOURCES

This application uses 633 of the 1024 available instruction words in the Flash program memory. Dynamically, the application uses up to 44 bytes of the 64 bytes available.

## CONCLUSION

This application note has shown how a PIC12HV615 MCU can be used to implement a digital current control loop for power LEDs. The integrated peripherals of the PIC12HV615 allow a low-cost implementation with room for additional features. These features include dimming of the LED, temperature regulation, and communication functions.

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**APPENDIX A: SOURCE CODE**

```
#include <12F615.h>
#include "pi.h"

#fuses INTRC_IO,NOPROTECT
#fuses IOOSC8,MCLR,BROWNOUT_NOSL,NOWDT
#fuses PUT,BROWNOUT

#device ADC = 10           // ADC library will return 10-bit ADC result

// Variable declarations
tPIParams Current;        // Data Structure for PI controller. See pi.h

int Count1msec;            // Software count for scheduling PI calculation
int1 Event1msec;           // Flag to indicate time for PI calculation

//Function Prototypes
void Setup(void);

//-----
// The Timer2 ISR will be invoked at a 7.8 kHz rate with Fosc = 8MHz.
// A count variable is incremented in the ISR and a flag is set every
// 16 counts that will trigger the PI calculations. The PI controller
// is therefore executed at 7.8kHz/8 = 976 Hz.
//-----
#define INT_TIMER2
void timer2_isr()
{
    Count++;
    if(Count == 8)
    {
        Count1msec = 0;
        Event1msec = 1;
    }
}
```

```
-----  
// The device code begins here. After the peripherals and variables  
// are initialized, the StartPI flag is polled in an endless loop.  
-----  
  
void main()  
{  
    // Setup peripheral functions  
    Setup();  
  
    // Setup gains and initial values for the PI controller  
    // Note: The value of Current.Setpoint will depend on the  
    // gain of the current feedback circuit.  
    Current.Kp = 35;  
    Current.Ki = 2;  
    Current.OutMax = 50;  
    Current.Setpoint = 100;  
    Current.Feedback = 0;  
    Current.Integral = 0;  
  
    while(1)  
    {  
        // Poll for flag  
        if(Event1msec)  
        {  
            // Read ADC to get current feedback value. The present  
            // sample is averaged with the previous sample.  
            Current.Feedback += read_adc();  
            Current.Feedback /= 2;  
            // Calculate the PI controller using variables in the  
            // 'Current' data structure.  
            CalcPI(&Current);  
            // Write the calculated PWM duty cycle to the CCP module.  
            set_pwm1_duty(Current.Output);  
            // Clear the flag  
            Event1msec = 0;  
        }  
    }  
}  
-----  
  
void Setup(void)  
{  
    set_tris_a(0xfb);           // GP2 is output for PWM  
    setup_ccp1(CCP_PWM);       // Enable CCP module for PWM  
    set_pwm1_duty(0);          // Set initial PWM duty cycle  
    setup_timer_2(T2_DIV_BY_1,0x0f,16); // Enable TMR2 with /16 postcaler  
  
    // Note: AN0, AN1, and AN3 are enabled as analog inputs. Although  
    // not required, the AN1 and AN3 inputs can be used to monitor  
    // parameters such as temperature, bus voltage, or LED forward  
    // voltage.  
  
    setup_adc_ports(sAN0 | sAN1 | sAN3); // AN0,AN1,AN3 analog inputs  
    setup_adc(ADC_CLOCK_INTERNAL);     // enable ADC - internal clk  
    set_adc_channel(0);               // input channel AN0  
  
    enable_interrupts(INT_TIMER2);    // Enable timer interrupts  
    enable_interrupts(GLOBAL);       // Enable CPU interrupts  
}
```

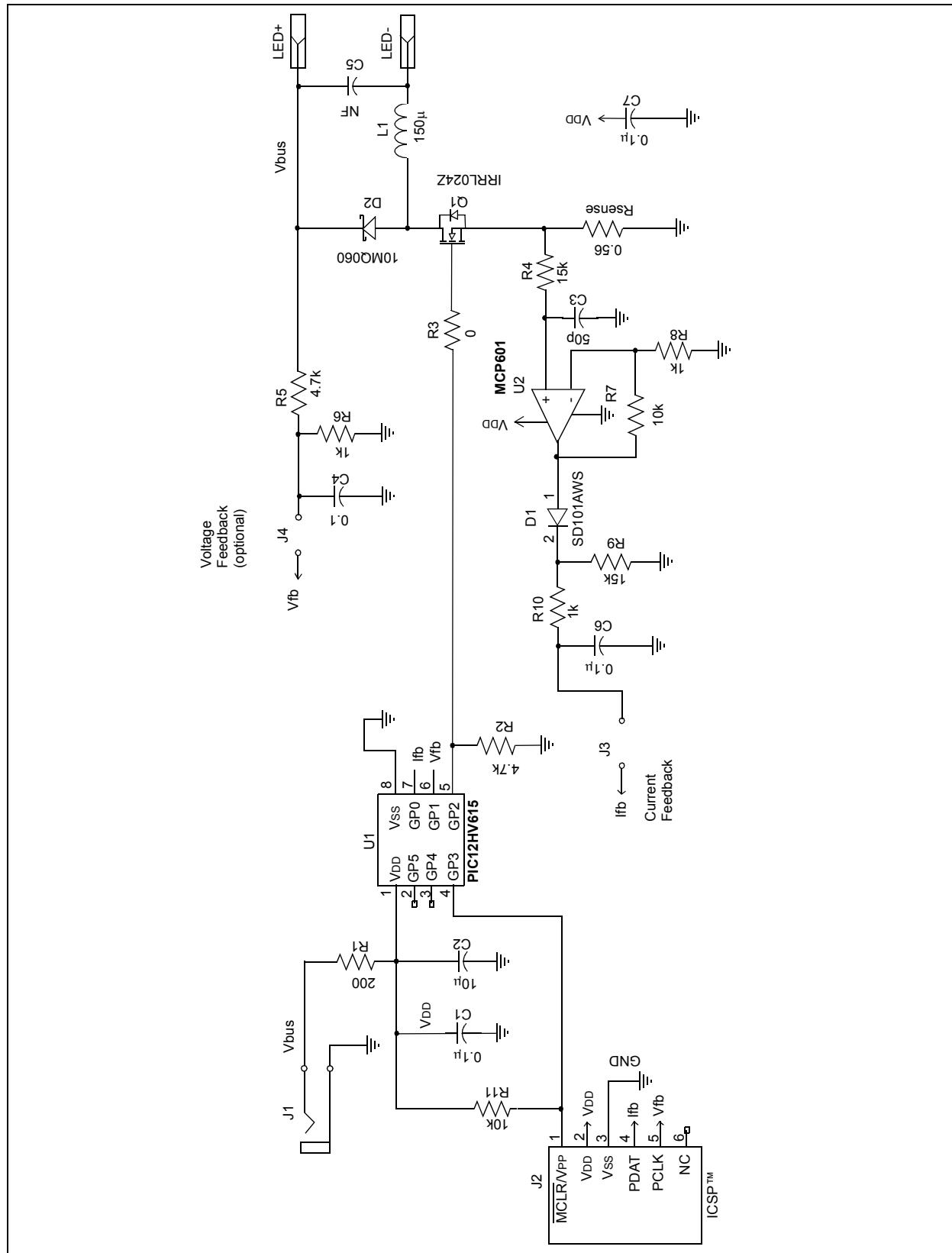
```
void CalcPI(tPIParams *PIdata)
{
    PIdata->Error = PIdata->Setpoint - PIdata->Feedback;
    // Deadband -- If the magnitude of the error is 2 or less,
    // then don't calculate the PI routine at all. This saves
    // processor time and avoids oscillation problems.
    if((PIdata->Error > 2) || (PIdata->Error < -2))
    {
        // If the PI controller is saturated, then don't do any
        // accumulation of the integral.
        if(PIdata->Saturated == 0)
        {
            // Do some boundary checking on the integral value
            // to avoid overflow. If the integral value is near
            // the limits, then we won't do the accumulation.
            if(PIData->Error > 0)
            {
                if(PIData->Integral < 32000)
                    PIdata->Integral += PIdata->Error;
                }
                else
                {
                    if(PIData->Integral > -32000)
                        PIdata->Integral += PIdata->Error;
                    }
                }
            // Now, calculate the actual PI function here.
            PIdata->Output = (PIdata->Error * PIData->Kp \
            + PIdata->Integral * PIdata->Ki)/256;

            // Perform boundary checks on the PI controller output. If the
            // output limits are exceeded, then set output to the limit
            // and set flag.
            if(PIdata->Output > PIdata->OutMax)
            {
                PIdata->Saturated = 1;
                PIdata->Output = PIdata->OutMax;
            }

            else if(PIdata->Output < 0)
            {
                PIdata->Saturated = 1;
                PIdata->Output = 0;
            }
            else PIdata->Saturated = 0;
        }
    }
}
```

## APPENDIX B: LED DRIVER DEMO SCHEMATIC

FIGURE B-1: SCHEMATIC



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Fax: 34-91-708-08-91

**UK - Wokingham**  
Tel: 44-118-921-5869  
Fax: 44-118-921-5820